Phase Diagram Data for Several PEG + Salt Aqueous Biphasic Systems at 25 $^{\circ}\text{C}$

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Phase diagrams determined by the cloud point method at 25 °C, including tie lines assigned from mass phase ratios according to the lever arm rule, are presented for several poly(ethylene glycol) (PEG) + salt aqueous biphasic systems (ABS). The systems include PEG-1000 + K_3PO_4 , PEG-2000 + K_3PO_4 , PEG-3400 + K_3PO_4 , and PEG-2000 in combination with the following salts K_2CO_3 , (NH₄)₂SO₄, Li₂SO₄, ZnSO₄, MnSO₄, and NaOH.

Introduction

Aqueous biphasic systems (ABS), also known as aqueous two-phase systems, have been applied for over 40 years to the separation, fractionation, and molecular characterization of biological macromolecules and particles.¹⁻⁵ Applications to protein purification at industrial scales have been discussed in the literature over the last 25 years.^{6,7} Despite strong efforts to improve adsorption steps in industrial bioprocessing, ABS are still seen to have considerable advantages in the early stages of biorecovery processes, especially with regard to efficient throughput and space-time yield.⁸ During the same time frame, applications of ABS to biotransformations have also been the subject of some interest.^{9,10} In more recent years, increasingly diverse applications of ABS have appeared in the literature. These include applications to the recovery of metal ions and radiochemicals;^{11–13} applications in the recovery of dyes, drug molecules, and small organic species;^{14–17} and applications to the recovery of inorganic particles.¹⁸ A yet more recent emerging trend has been the investigation of ABS as an alternative solvent system for chemical reactions. Processes employing ABS have been demonstrated in the recovery of lignin and cellulose during paper pulping.^{19,20} Aqueous biphasic reactive extraction (ABRE) processes employing alkaline earth metal catalysts for delignification in paper pulping have been demonstrated.²¹ Most recently, an ABRE process was demonstrated for the conversion of cyclohexene to adipic acid in a reaction employing hydrogen peroxide and a tungstate catalyst.²² These latest developments suggest the opening of a new phase in the development of applied ABS processes.

Undoubtedly, commercial applications of ABS have been slow to develop, for which a number of reasons may be adduced. Development of processes still appears to be heuristic, and there are currently no suppliers of specific applications or products, as is ubiquitously found for adsorption processes. Recycling of phases is perceived as far more problematic than that for aqueous + organic systems. On the other hand, chemical and water usage is

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beginning to seem more problematic in process chromatography steps as well. $^{\rm 23}$

By now there is considerable data in the literature relating to the operation of ABS, including phase diagrams, their physical chemistry, and the purification of particular products. We present here some phase diagrams of PEG + salt ABS that have not been previously published. Some other sources of phase diagram data for ABS should, perhaps, be mentioned here. Albertsson's seminal monograph is, of course, well-known.¹ The book by Zaslavsky contains a summary of most of the phase diagram data available at that time.⁴ Considerable new and useful phase diagram data have appeared in the literature since including, but not comprehensively, data relating to PEG + salt systems,^{24–27} to PEG + dextran systems,^{28–30} and to systems employing copolymers.^{31,32}

Methods

The salts (NH₄)₂SO₄, K₃PO₄, K₂CO₃, Li₂SO₄, MnSO₄, NaOH, and ZnSO₄ and the polymers PEG-1000, PEG-2000, and PEG-3400 used were obtained from Aldrich (Milwaukee, WI) and were of reagent grade. Water was obtained from a commercial deionization system (Barnsted, Dubuque, IA). For the preparation of phase diagrams, stock solutions of polymer and salt were prepared on a mass percent basis. Phase diagrams were determined by the cloud point method³³ and fitted by least squares regression to an empirical relationship developed by Merchuk³⁴ and shown in eq 1. Measurements of mass for the preparation of stock solutions and for the determination of cloud points were made in grams on a top loading balance to four significant figures. Compositions were then calculated and reduced to two significant figures prior to the fitting of binodals and tie lines.

$$Y_{\rm A} = a \exp(bX_{\rm A}^{0.5} - cX_{\rm A}^{-3}) \tag{1}$$

where Y_A and X_A are the concentrations of polymer and salt, respectively, which had been determined to lie on the cloud point curve. Tie lines for each ABS were assigned by application of the lever arm rule to the relationship between the mass phase composition and the overall



Figure 1. Phase diagram in w/w % of the PEG-1000 (1) + K_3PO_4 (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.

Table 1. Empirical Coefficients of Eq 1 for Various PEG+ Salt ABS

	system	а	b	С	I^2
1	K ₃ PO ₄ /PEG-1000	63.40	-0.3242	4.285×10^{-4}	0.9998
2	K ₃ PO ₄ /PEG-2000	115.88	-0.6685	$5.727 imes 10^{-4}$	0.9992
3	K ₃ PO ₄ /PEG-3400	77.35	-0.5213	$1.141 imes 10^{-3}$	0.9998
4	K ₂ CO ₃ /PEG-2000	124.20	-0.5589	$9.392 imes 10^{-4}$	0.9991
5	(NH ₄) ₂ SO ₄ /PEG-2000	87.41	-0.4360	$4.303 imes 10^{-4}$	0.9988
6	Li ₂ SO ₄ /PEG-2000	73.98	-0.3444	$6.590 imes 10^{-4}$	0.9996
7	MnSO ₄ /PEG-2000	65.65	-0.4293	$2.671 imes 10^{-4}$	0.9997
8	ZnSO ₄ /PEG-2000	70.69	-0.4542	$2.970 imes 10^{-4}$	0.9918
9	NaOH/PEG-2000	105.79	-0.5572	2.346×10^{-3}	0.9990

system composition. Details of the mathematical methods used are given elsewhere.^{15,34} The phase relationships were also placed on a molal basis by conversion of the mass percent data (data not shown).

Cloud point data for systems composed of different salt types were also fitted to the statistical geometrical relationship of Lilley³⁵ shown in eq 2:

$$w_1 = -\ln\left(V^* \frac{w_2}{M_2}\right) \frac{M_1}{V^*}$$
(2)

where w_1 is the salt concentration, w_2 is the polymer concentration, M_2 and M_1 are the polymer and salt molar masses, and V^* is the scaled excluded volume. As noted by Lilley, because of the variation in the density along the cloud point curve, this is an empirical application of the statistical geometry approach. The interest lies in the behavior of the single fitted parameter of eq 2 in systems formed with a variety of different salts.

Results

Phase diagrams for the various PEG + salt systems examined here are shown in Figures 1–9. The binodal curves have been fitted according to the empirical relationship of Merchuk,³⁴ and the coefficients for this regression as determined by least squares regression of the cloud point data are shown in Table 1. The raw cloud point data (to two significant figures) for these systems are given in Table 2 so that fitting by other mathematical or thermodynamic relationships is enabled. While Figures 1–9 and the regression coefficients in Table 1 indicate that the empirical equation (eq 1) gives a rather good fit to the data for



Figure 2. Phase diagram in w/w % of the PEG-2000 (1) + K_3PO_4 (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.



Figure 3. Phase diagram in w/w % of the PEG-3400 (1) + K_3PO_4 (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.



Figure 4. Phase diagram in w/w % of the PEG-2000 (1) + K_2 -CO₃ (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.

descriptive purposes, it is in many ways deficient. The exact form of the data and, perhaps, the way it has been collected



Figure 5. Phase diagram in w/w % of the PEG-2000 $(1) + (NH_4)_2$ -SO₄ (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.

result in an interplay between the various coefficients such that there is little systematic variation which could be used in deriving a general description of a PEG + salt binodal curve which was independent of salt type and polymer molecular weight.

Tie lines for these cloud point curves were fitted by a least-squares method based on the lever arm rule described



Figure 6. Phase diagram in w/w % of the PEG-2000 (1) + Li_2 -SO₄ (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.

previously,¹⁵ and these are shown in Figures 1-9. Numerical data for these tie lines are given in Table 3. The average slope of the tie lines is also shown in Table 3. As may be seen from these data and from Figures 1-9, the slope of the tie lines is approximately constant at short tie line lengths but there is significant change in tie line slope as tie line length increases. This is probably due to the fact

Table 2. Experimentally Determined Cloud Points for PEG (1) + Salt (2) + Water (3)

$\frac{\text{PEG-1000}+}{\text{K}_3\text{PO}_4}$		PEG-2 K ₃ I	$2000 + PO_4$	PEG-3 K ₃ I	$8400 + PO_4$	PEG-2 K ₂ ($2000 + CO_3$	PEG-2 (NH4	$2000 + 0_2 SO_4$	PEG-2 Li ₂	$2000 + SO_4$	PEG-2 Mn	$2000 + SO_4$	PEG-2 ZnS	$\begin{array}{r} 000 + PEG-200 \\ SO_4 NaOH \end{array}$		2000 + OH
$100 w_2$	$100 w_1$	$100 W_2$	$100 w_1$	$100 W_2$	$100 w_1$	$100 W_2$	$100 w_1$	$100 W_2$	$100 w_1$	100 <i>w</i> ₂	$100 w_1$	100 <i>w</i> ₂	$100 w_1$	$100 W_2$	$100 w_1$	$100 w_2$	$100 w_1$
4.12	32.12	2.85	37.15	3.27	29.23	5.44	29.52	3.79	36.21	4.34	34.20	3.96	27.74	1.85	37.53	2.39	43.92
5.94	26.55	3.56	33.15	4.21	24.09	6.28	24.23	5.35	31.56	5.93	28.00	5.25	23.35	4.60	29.52	3.33	34.27
6.26	24.88	4.03	29.26	5.33	19.18	6.75	20.03	5.71	28.39	8.64	17.00	7.30	18.20	4.75	23.86	4.41	26.02
7.15	22.34	4.32	25.93	6.50	14.76	7.65	17.82	6.45	25.08	10.97	10.53	9.03	14.82	6.64	18.95	5.59	18.99
8.12	19.89	5.35	22.89	7.66	11.35	8.06	16.08	7.34	21.83	12.41	6.56	10.49	12.18	8.05	15.69	6.45	14.32
8.78	18.05	5.54	21.16	8.60	8.73	8.37	14.39	8.16	19.35	12.91	5.54	11.07	11.16	10.80	11.23	6.70	12.96
9.60	16.03	6.08	19.02	9.22	6.86	8.57	13.22	8.89	17.09	12.96	5.12	11.76	9.95	12.06	8.80	6.90	11.86
10.44	13.96	6.64	17.09	9.73	5.44	8.84	12.52	9.62	15.11	13.19	4.74	12.57	8.55	13.41	6.77	7.14	10.67
10.93	12.69	7.28	15.32	10.18	4.32	9.14	11.70	10.20	13.33	13.32	4.45	13.00	7.86	14.48	5.03	7.37	9.51
11.41	11.40	8.04	13.63	10.56	3.52	9.44	11.11	10.78	13.29	13.49	4.11	13.51	7.04	15.84	3.60	7.59	8.41
12.05	9.96	8.41	12.20	10.60	3.39	9.53	10.41	10.45	13.28	13.63	3.87	13.85	6.54	17.20	2.52	7.88	7.04
12.17	9.55	8.96	10.72	10.84	2.90	9.54	9.96	11.02	11.84	13.84	3.57	14.19	6.06	18.05	1.82	8.04	6.30
12.47	8.87	9.54	9.37	11.62	1.63	9.57	9.64	11.61	10.50	13.92	3.40	14.59	5.53	21.56	0.30	8.23	5.46
12.79	8.19	10.15	8.14	12.66	1.05	9.76	9.32	12.10	9.33	14.04	3.21	14.89	5.11			8.38	4.80
13.11	7.60	10.54	7.04	13.06	0.96	9.77	9.06	12.61	8.16	14.12	3.04	15.37	4.51			8.96	2.79
13.31	7.10	11.01	5.93	13.38	0.91	9.74	8.80	13.04	7.12	14.19	2.92	15.84	4.06			9.35	2.00
13.54	6.62	11.30	5.92			9.81	8.63	13.68	6.22	14.36	2.72	16.92	2.95			10.07	1.04
13.83	6.11	11.55	5.40			9.90	8.41	14.04	5.49	14.37	2.50	17.94	2.08			10.77	0.71
14.01	5.70	11.70	4.87			9.94	8.21	14.40	4.81	14.73	2.10	18.18	2.10				
14.26	5.29	12.02	4.23			10.31	7.70	14.72	4.15	15.41	1.64	19.36	1.38				
14.50	4.91	12.38	3.75			10.41	7.40	15.09	3.57	16.10	1.00	19.73	1.24				
14.89	4.22	12.77	3.31			10.47	5.59	15.44	2.99	17.30	0.84	21.27	0.87				
15.27	3.67	12.86	2.91			11.01	4.24	15.88	2.23	19.75	0.48	22.14	0.48				
15.65	3.19	13.06	2.53			13.15	2.10	16.47	1.67								
16.17	2.67	13.24	2.18			13.43	1.81	17.13	1.31								
16.87	1.90	13.54	1.85			13.77	1.48	17.74	0.93								
17.64	1.42	13.80	1.58			14.25	1.15	18.39	0.59								
20.69	0.701	14.20	1.59			14.83	0.80	18.75	0.35								
		14.54	1.38			15.42	0.59	18.98	0.14								
		14.67	1.22			16.42	0.42	19.13	0.05								
		14.88	1.03					21.80	0.13								
		15.39	0.85														
		15.39	0.72														
		15.68	0.61														
		10.98	0.46														
		16.50	0.32														
		17.34	0.18														

Table 3. Tie Line Compositions of PEG (1) + Salt (2) + Water (3) Assigned by the Lever Arm Rule

PEG-1000 (1) + K_3PO_4 (2) + Water (3)									
		tie 1	tie	2	tie 3		tie 4		
$100w_1$ (mixture)		18.96	18 3	32	17 73		17 17		
$100 W_2$ (mixture)		9.43	13.6	36	17.62		21.34		
100 <i>w</i> ₁ (top)		30.02	43.1	12	49.88		56.04		
$100 w_1$ (bottom)		2.54	0.09)	$2.84 imes10^{-3}$		$4.33 imes10^{-5}$		
100 <i>w</i> ₂ (top)		4.70	1.40)	0.55		0.14		
$100 W_2$ (bottom)		16.44	22.0	58 D 4	27.11		30.70		
tie line length		29 89	0.44 48 (00	0.353		63 83		
tie line slope		-2.34	-2.	02	-1.88		-1.83		
1		DEC	$2000(1) \perp K.D$	$O_{1}(2) \pm Water (2)$					
	tio 1	rEC	$+1000(1) + K_3F$	$O_4(z) + \text{water (5)}$, 	tio F	tio 6		
	tie 1	tie 2	tie s	tie 4	Ł	tie 5	tie o		
$100 w_1$ (mixture)	18.88	18.24	17.60	17.09	16.5	56	16.36		
$100W_2$ (mixture) $100W_2$ (top)	9.46	13.72	17.69	21.41 54.60	24.9	11 02	28.20		
$100 w_1(top)$ $100 w_1(bottom)$	0.59	0.013	$\frac{49.03}{8.54 \times 10^{-5}}$	$^{-5}$ 2.16 ×	10^{-7} 3.98	3×10^{-10}	1.25×10^{-13}		
$100 w_2(top)$	3.02	2.022	1.58	1.26	0.96	3	0.83		
100 <i>w</i> ₂ (bottom)	16.47	21.81	26.52	30.60	33.9	99	37.57		
phase ratio (mass)	0.521	0.409	0.354	0.313	0.27	75	0.255		
tie line length	37.58	48.76	55.73	61.98	68.7	70	72.98		
tie line slope	-2.61	-2.25	-2.00	-1.86	-1.3	82	-1.72		
		PEC	$-3400(1) + K_3P$	$O_4(2) + Water(3)$)				
		tie 1	tie	2	tie 3		tie 4		
100w1(mixture)		18.97	18.33		17.74		17.18		
100w2(mixture)		9.42	13.66		17.62		21.33		
100 <i>w</i> ₁ (top)		36.64	45.35	_	50.44		55.45		
$100 w_1$ (bottom)		0.02	$2.44 \times$	10^{-5}	$1.48 imes 10^{-9}$		$1.85 imes 10^{-14}$		
$100 w_2(top)$ $100 w_2(bottom)$		2.00	1.04		0.67		0.41		
nhase ratio (mass)		0.517	0 404		0 352		0 310		
tie line length		39.71	50.05		56.81		63.19		
tie line slope	tie line slope -2.38		-2.14	-2.14 -			-1.83		
		PEC	-2000 (1) + K ₂ C	O ₂ (2) + Water (3))				
	tie 1	PEC	$-2000 (1) + K_2C$ tie 3	$O_3(2) + Water(3)$)	tie 5	tie 6		
100 <i>w</i> (mixture)	tie 1	PEC tie 2	$-2000 (1) + K_2C$ tie 3	$O_3(2) + Water(3)$ tie 4) L 173	tie 5	tie 6		
	tie 1 19.07 9.34	PEC tie 2 18.70 12.21	$\frac{-2000 (1) + K_2C}{\text{tie 3}}$ $\frac{18.35}{14.97}$	$ O_{3}(2) + Water (3) tie 4 17.68 20.19 $) I 17.3 22.6	tie 5 34 37	tie 6		
$100 w_1 (mixture)$ $100 w_2 (mixture)$ $100 w_1 (top)$	tie 1 19.07 9.34 31.57	PEC tie 2 18.70 12.21 41.73	$ \frac{-2000 (1) + K_2C}{\text{tie 3}} \\ \frac{18.35}{14.97} \\ 46.22 $	$\frac{O_3 (2) + \text{Water } (3)}{\frac{\text{tie } 2}{17.68}}$ 20.19 57.76) 1 17.3 22.6 59.5	tie 5 34 37 59	tie 6 17.05 25.05 64.59		
100 <i>w</i> ₁ (mixture) 100 <i>w</i> ₂ (mixture) 100 <i>w</i> ₁ (top) 100 <i>w</i> ₁ (bottom)	tie 1 19.07 9.34 31.57 0.33	PEC tie 2 18.70 12.21 41.73 0.01	$\frac{1.2000 (1) + K_2C}{\frac{\text{tie 3}}{18.35}}$ $\frac{18.35}{14.97}$ $\frac{46.22}{1.14 \times 10^{-3}}$	$\begin{array}{r} \text{O}_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ \hline \\ -4 \\ 3.78 \times \end{array}$	1 17.3 22.6 59.5 10^{-9} 1.77	tie 5 34 37 59 7×10^{-12}	tie 6 17.05 25.05 64.59 1.98 × 10 ⁻¹⁵		
100 <i>w</i> ₁ (mixture) 100 <i>w</i> ₂ (mixture) 100 <i>w</i> ₁ (top) 100 <i>w</i> ₁ (bottom) 100 <i>w</i> ₂ (top)	tie 1 19.07 9.34 31.57 0.33 5.01	PEC tie 2 18.70 12.21 41.73 0.01 3.53		$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ $	1 17.3 22.6 59.5 10^{-9} 1.77 1.70	tie 5 34 37 59 7×10^{-12} 0	$\begin{array}{r} tie \ 6\\ \hline 17.05\\ 25.05\\ 64.59\\ 1.98\times 10^{-15}\\ 1.36\end{array}$		
100 <i>w</i> ₁ (mixture) 100 <i>w</i> ₂ (mixture) 100 <i>w</i> ₁ (top) 100 <i>w</i> ₁ (bottom) 100 <i>w</i> ₂ (top) 100 <i>w</i> ₂ (bottom)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.42	$\begin{array}{c} -2000 \ (1) + K_2 C \\ \hline \\ \hline \\ \hline \\ 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 22.87 \\ 22.97 \end{array}$	$O_{3}(2) + Water (3)$ 17.68 20.19 57.76 $3.78 \times$ 1.85 28.28 2.920	1 17.3 22.6 59.5 10^{-9} 1.77 1.70 31.2 2.62 2.62 2.62 3.62 2.62	tie 5 34 57 7×10^{-12} 28	$\begin{array}{r} \text{tie 6} \\ \hline 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.044 \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{phase ratio (mass)}}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 23.06	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58	$\begin{array}{r} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50 \ 21 \end{array}$	$O_{3}(2) + Water (3)$ 17.68 20.19 57.76 -4 $3.78 \times$ 1.85 28.28 0.306 62.52	1 17.3 22.6 59.5 10 ⁻⁹ 1.77 1.70 31.2 0.25 66 5	tie 5 34 37 59 7×10^{-12} 28 31 52	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72, 168 \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{phase ratio (mass)}}$ $\frac{100 w_2(\text{bottom})}{100 w_2(\text{bottom})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65	$\begin{array}{r} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ $	$1 \\ 17.3 \\ 22.6 \\ 59.5 \\ 10^{-9} \\ 1.77 \\ 1.70 \\ 31.2 \\ 0.29 \\ 66.5 \\ -2.1 \\ 0.21 \\ 0.22 \\ 0.21 \\ 0.21 \\ 0.22 \\ 0.21 \\ $	tie 5 34 57 7×10^{-12} 28 91 53 01	$\begin{array}{r} tie \ 6 \\ \hline 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{mixture})}{100 w_1(\text{top})}$ $\frac{100 w_1(\text{bottom})}{100 w_2(\text{top})}$ $\frac{100 w_2(\text{bottom})}{100 w_2(\text{bottom})}$ phase ratio (mass) tie line length tie line slope	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65	$\begin{array}{r} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \end{array}$	$1 \\ 17.3 \\ 22.6 \\ 59.5 \\ 10^{-9} \\ 1.77 \\ 1.76 \\ 31.2 \\ 0.29 \\ 66.5 \\ -2.6 \\ 0.21 \\ 0.22 \\ $	tie 5 34 57 59 7×10^{-12} 28 91 53 01	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{mixture})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{phase ratio (mass)}}$ $\frac{100 w_2(\text{bottom})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{100 w_2(\text{bottom})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2	$\begin{array}{c} -2000 \ (1) \ + \ K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) \ + \ (NH_4); \end{array}$	$O_{3}(2) + Water (3)$ $tie 4$ 17.68 20.19 57.76 -4 $3.78 \times$ 1.85 28.28 0.306 63.53 -2.18 $2SO_{4}(2) + Water$	$ \begin{array}{c} 17.3 \\ 22.6 \\ 59.5 \\ 10^{-9} \\ 1.77 \\ 1.70 \\ 31.2 \\ 0.29 \\ 66.5 \\ -2.0 \\ (3) \end{array} $	$\frac{\text{tie 5}}{37}$ $\frac{34}{59}$ 7×10^{-12} $\frac{28}{53}$ 01	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{phase ratio (mass)}}$ $\frac{\text{tie line length}}{\text{tie line slope}}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1	$\begin{array}{c} -2000 \ (1) \ + \ K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) \ + \ (NH_4); \\ \hline tie \ 2 \end{array}$	$O_{3}(2) + Water (3)$ $tie 4$ 17.68 20.19 57.76 -4 $3.78 \times$ 1.85 28.28 0.306 63.53 -2.18 $2SO_{4}(2) + Water$ $tie 3$	$ \begin{array}{c} 17.3 \\ 22.6 \\ 59.5 \\ 10^{-9} \\ 1.77 \\ 1.76 \\ 31.2 \\ 0.22 \\ 66.5 \\ -2.6 \\ (3) \\ \hline \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ \\ $	tie 5 34 57 59 7×10^{-12} 28 31 53 01 4	tie 6 17.05 25.05 64.59 1.98 × 10 ⁻¹⁵ 1.36 33.54 0.264 72.168 -2.01 tie 5		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_2(\text{mixture})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{tie line length}}$ $\frac{100 w_1(\text{mixture})}{100 w_1(\text{mixture})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5	$\begin{array}{c} -2000 \ (1) \ + \ K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) \ + \ (NH_4); \\ \hline tie \ 2 \\ \hline 19.29 \\ 19.29 \\ \hline \end{array}$	$O_{3}(2) + Water (3)$ $tie 4$ 17.68 20.19 57.76 -4 $3.78 \times$ 1.85 28.28 0.306 63.53 -2.18 $2SO_{4}(2) + Water$ $tie 3$ 19.17 19.17	$ \frac{1}{10^{-9}} $ $ \frac{17.3}{1.70} $ $ \frac{10^{-9}}{1.77} $ $ \frac{1.77}{1.70} $ $ \frac{1.2}{66.5} $ $ -2.0 $ $ \frac{(3)}{18.80} $	$\frac{\text{tie 5}}{37}$ $\frac{37}{59}$ 7×10^{-12} $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \text{tie 5} \\ 18.57 \\ 18.57 \\ \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{tie line length}}$ $\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.22 22.4	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3	$\begin{array}{c} -2000 \ (1) \ + \ K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) \ + \ (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.00 \\ \end{array}$	$O_{3}(2) + Water (3)$ 17.68 20.19 57.76 -4 $3.78 \times$ 1.85 28.28 0.306 63.53 -2.18 $2SO_{4}(2) + Water$ 19.17 15.62 46.00	$ \frac{1}{10^{-9}} = \frac{17.3}{1.77} \\ 10^{-9} = \frac{1.77}{1.70} \\ 1.76 \\ 31.2 \\ 0.22 \\ 66.5 \\ -2.6 \\ (3) \\ \hline 18.80 \\ 18.55 \\ 48.95 \\ 48.95 \\ 18.55 \\ 49.97 \\ 18.55 \\ 18.55 \\ 49.97 \\ 18.55 $		$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \text{tie 5} \\ 18.57 \\ 21.43 \\ 52.07 \\ \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{tie line length}}$ $\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{top})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28O_{4}\left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 28O_{4}\left(2\right) + \text{Water} \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \end{array}$	$ \begin{array}{c} 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\ 1 \\$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$ $\frac{31}{53}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \text{tie 5} \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \end{array}$		
$\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{top})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{bottom})}$ $\frac{100 w_2(\text{bottom})}{\text{tie line length}}$ $\frac{100 w_1(\text{mixture})}{100 w_2(\text{mixture})}$ $\frac{100 w_1(\text{pottom})}{100 w_1(\text{bottom})}$ $\frac{100 w_2(\text{top})}{100 w_2(\text{top})}$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right)\\ \hline \\ \hline \\ \hline \\ 17.68\\ 20.19\\ 57.76\\ 3.78 \times \\ 1.85\\ 28.28\\ 0.306\\ 63.53\\ -2.18\\ \hline \\ 2\text{SO}_{4}\left(2\right) + \text{Water}\\ \hline \\ \hline \\ \hline \\ \frac{19.17}{15.62}\\ 46.00\\ 9.52 \times 10^{-3}\\ 2.14 \end{array}$	$\begin{array}{c} 17.3\\ 22.6\\ 59.5\\ 10^{-9} & 1.77\\ 1.70\\ 31.2\\ 0.22\\ 66.5\\ -2.0\\ (3)\\ \hline \\ \hline \\ 18.80\\ 18.55\\ 48.97\\ 2.27 \times 1\\ 1.75\\ \hline \end{array}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{31}{53}$ $\frac{31}{5$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ \text{tie 5} \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ \end{array}$		
100 w_1 (mixture) $100 w_2$ (mixture) $100 w_1$ (bottom) $100 w_2$ (top) $100 w_2$ (bottom)phase ratio (mass)tie line lengthtie line slope100 w_1 (mixture) $100 w_2$ (mixture) $100 w_2$ (mixture) $100 w_1$ (bottom) $100 w_2$ (top) $100 w_2$ (top) $100 w_2$ (top) $100 w_2$ (top) $100 w_2$ (bottom)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right)\\ \hline \\ \hline \\ \hline \\ 17.68\\ 20.19\\ 57.76\\ 3.78 \times \\ 1.85\\ 28.28\\ 0.306\\ 63.53\\ -2.18\\ \hline \\ 2\text{SO}_{4}\left(2\right) + \text{Water}\\ \hline \\ \hline \\ \hline \\ \hline \\ 19.17\\ 15.62\\ 46.00\\ 9.52 \times 10^{-3}\\ 2.14\\ 25.26\\ \hline \end{array}$	$\begin{array}{c} 17.3\\ 22.6\\ 59.5\\ 10^{-9} \\ 1.77\\ 1.70\\ 31.2\\ 0.29\\ 66.5\\ -2.0\\ (3) \\ \hline \\ \hline \\ 18.80\\ 18.55\\ 48.97\\ 2.27 \times 1\\ 1.75\\ 29.02 \end{array}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{31}{53}$ 01 $\frac{4}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ \end{array}$		
$100 w_1$ (mixture) $100 w_2$ (mixture) $100 w_1$ (top) $100 w_1$ (bottom) $100 w_2$ (top) $100 w_2$ (bottom)phase ratio (mass)tie line lengthtie line slope $100 w_2$ (mixture) $100 w_2$ (mixture) $100 w_1$ (top) $100 w_1$ (bottom) $100 w_2$ (bottom) $phase ratio (mass)$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1 0.59	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ \hline \end{array}$	$\begin{array}{c} 17.3\\ 22.6\\ 59.5\\ 10^{-9} \\ 1.77\\ 1.76\\ 31.2\\ 0.29\\ 66.5\\ -2.4\\ (3) \\ \hline \\ 18.80\\ 18.55\\ 48.97\\ 2.27 \times 1\\ 1.75\\ 29.02\\ 0.384 \\ \end{array}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{31}$ $\frac{31}{53}$ $\frac{1}{10^{-4}}$	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ \end{array}$		
$100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(bottom)$ $100 w_2(bottom)$ $phase ratio (mass)$ tie line length	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5 10.2 32.4 1.04 4.72 18.1 0.59 34.1	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ \hline 0.12 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ \hline 0.12 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ 0.12 \\ 0.13 \\ 0.470 \\ 0.13 \\ 0.470 \\ 0.14 \\$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 25.26 \\ 0.417 \\ 51.44 \\ 0.02 \\$	$\begin{array}{c} 17.3\\ 22.6\\ 59.5\\ 10^{-9} \\ 1.77\\ 1.70\\ 31.2\\ 0.29\\ 66.5\\ -2.1\\ (3)\\ \hline \\ 18.80\\ 18.55\\ 48.97\\ 2.27 \times 1\\ 1.75\\ 29.02\\ 0.384\\ 56.04\\ 56.04\end{array}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{31}{53}$ 01 $\frac{4}{10^{-4}}$	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ 1.51 \\ \hline \\ \end{array}$		
$100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_2(bottom)$ phase ratio (mass)tie line lengthtie line slope $100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_2(top)$ $100 w_2(top)$ $100 w_2(top)$ $100 w_2(top)$ $100 w_2(top)$ $100 w_2(bottom)$ phase ratio (mass)tie line lengthtie line slope	$\begin{array}{c} \text{tie 1} \\ 19.07 \\ 9.34 \\ 31.57 \\ 0.33 \\ 5.01 \\ 15.82 \\ 0.600 \\ 33.06 \\ -2.89 \\ \hline \\ \hline \\ 19.5 \\ 10.2 \\ 32.4 \\ 1.04 \\ 4.72 \\ 18.1 \\ 0.59 \\ 34.1 \\ -2.3 \\ \end{array}$	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 3 1 5 3 1	$\begin{array}{c} -2000 \ (1) + K_2 C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4); \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \end{array}$	$\begin{array}{c} 1 \\ 1 \\ 22.6 \\ 59.5 \\ 10^{-9} \\ 1.77 \\ 1.70 \\ 31.2 \\ 0.29 \\ 66.5 \\ -2.1 \\ (3) \\ \hline \\ 18.80 \\ 18.55 \\ 48.97 \\ 2.27 \times 1 \\ 1.75 \\ 29.02 \\ 0.384 \\ 56.04 \\ -1.80 \\ \end{array}$	$\frac{\text{tie 5}}{59}$ 7 × 10 ⁻¹² 28 31 53 01 4 10 ⁻⁴	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \end{array}$		
$100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_2(bottom)$ phase ratio (mass) tie line length tie line slope $100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_1(bottom)$ $100 w_2(bottom)$ $phase ratio (mass)$ tie line length tie line slope	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5 10.2 32.4 1.04 4.72 18.1 0.59 34.1 -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 5 0 2 83 PEC	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{\circ} \\ 2.97 \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4); \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water }\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28O_{4}\left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 28O_{4}\left(2\right) + \text{Water} \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water} \left(3\right) \\ \hline \\ \end{array}$	$\begin{array}{c} & & & & \\ & & & & & \\ & & & & & \\ & & & & & \\ 10^{-9} & & & & 1.77 \\ & & & & & \\ 1.76 \\ & & & & & \\ & & & & & \\ 0.25 \\ & & & & & \\ 66.5 \\ & & & & & \\ -2.0 \\ \hline & & & & \\ (3) \\ \hline & & & & & \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & & \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & & \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & & & \\ \hline & & & & \\ (3) \\ \hline & & \\ (3) $	$\frac{\text{tie 5}}{34}$ $\frac{34}{59}$ 7×10^{-12} $\frac{28}{53}$ 01 $\frac{4}{10^{-4}}$	$\begin{array}{r} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ \text{tie 5} \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \end{array}$		
$100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_2(top)$ $100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(top)$ $100 w_1(top)$ $100 w_2(top)$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1 0.59 34.1; -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 33 PEG tie 1	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water }\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water} \left(3 \\ \hline \\ \hline \\ \hline \\ 1000$	$\frac{1}{10^{-9}}$ $\frac{17.3}{1.22.6}{59.5}{59.5}{10^{-9}}$ $\frac{10.77}{1.70}$ $\frac{1.77}{1.70}$ $\frac{1.2}{66.5}{-2.1}$ $\frac{18.80}{18.55}$ $\frac{18.95}{48.97}$ $\frac{2.27 \times 1}{1.75}$ $\frac{2.9.02}{0.384}$ $\frac{56.04}{-1.80}$ $\frac{18.3}{100}$ $\frac{100}{100}$ $\frac{100}{100}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{31}$ $\frac{31}{53}$ $\frac{1}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ $		
$100 w_1(mixture)$ $100 w_2(mixture)$ $100 w_1(bottom)$ $100 w_2(top)$ $100 w_1(mixture)$ $100 w_1(top)$ $100 w_1(top)$ $100 w_2(top)$ $100 w_1(mixture)$	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1 0.59 34.1: -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 33 PEG tie 1 19.31	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water}\left(3 \\ \hline \\ \hline \\ 19.22 \\ \hline \end{array}$	$\begin{array}{c} & & & & & \\ & & & & & \\ 10^{-9} & & & & 1.77 \\ & & & & 59.5 \\ 10^{-9} & & & & 1.77 \\ & & & & 1.76 \\ & & & & & 0.29 \\ & & & & 66.5 \\ & & & & -2.6 \\ & & & & & -2.6 \\ \hline & & & & & & (3) \\ \hline & & & & & & & (3) \\ \hline & & & & & & & (3) \\ \hline & & & & & & & (3) \\ \hline & & & & & & & & (3) \\ \hline & & & & & & & & (3) \\ \hline & & & & & & & & & (3) \\ \hline & & & & & & & & & (3) \\ \hline & & & & & & & & & (3) \\ \hline & & & & & & & & & (3) \\ \hline & & & & & & & & & & (3) \\ \hline & & & & & & & & & & (3) \\ \hline & & & & & & & & & & (3) \\ \hline & & & & & & & & & & & (3) \\ \hline & & & & & & & & & & & (3) \\ \hline & & & & & & & & & & & & (3) \\ \hline & & & & & & & & & & & & & & & & (3) \\ \hline & & & & & & & & & & & & & & & & & &$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{31}$ $\frac{31}{53}$ $\frac{1}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ \hline \\ 19.00 \\ \hline \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line slope	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1 0.59 34.1: -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 33 PEG tie 1 19.31 8.53	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water}\left(3 \\ \hline \\ \hline \\ 19.22 \\ 8.98 \\ \hline \end{array}$	$\begin{array}{c} & & & & & \\ & & & & & \\ 10^{-9} & & & & & \\ 10^{-9} & & & & & \\ 1.77 \\ & & & & & \\ 0.29 \\ & & & & & \\ 66.5 \\ & & & & & \\ -2.0 \\ \hline & & & & \\ (3) \\ \hline \\ \hline & & & & \\ (3) \\ \hline \\ \hline & & & & \\ 18.80 \\ 18.55 \\ & & & & \\ 48.97 \\ 2.27 \times 1 \\ 1.75 \\ 29.02 \\ 0.384 \\ 56.04 \\ -1.80 \\ \hline \\ $	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{301}$ $\frac{31}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ \hline \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_2 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_1 (top)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2: 32.4 1.04 4.72 18.1 0.59 34.1: -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 33 PEG tie 1 19.31 8.53 25.84	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water}\left(3 \\ \hline \\ \hline \\ 19.22 \\ 8.98 \\ 30.94 \\ 9.90 \\ \hline \end{array}$	$\begin{array}{c} & & & & & \\ & & & & & \\ 10^{-9} & & & & 1.77 \\ & & & & 59.5 \\ 10^{-9} & & & & 1.77 \\ & & & & 1.76 \\ & & & & & 0.29 \\ & & & & 66.5 \\ & & & & -2.6 \\ & & & & & -2.6 \\ \hline & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & 18.80 \\ & & & & & & & & 18.80 \\ & & & & & & & 18.80 \\ & & & & & & & 18.80 \\ & & & & & & & & 18.80 \\ & & & & & & & & 18.80 \\ & & & & & & & & & 18.80 \\ & & & & & & & & & 18.80 \\ & & & & & & & & & & 18.80 \\ & & & & & & & & & & & 18.80 \\ & & & & & & & & & & & & & & & & & \\ &$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{31}$ $\frac{31}{53}$ $\frac{1}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ 38.64 \\ 2.52 \\ \hline \\ \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line slope 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_1 (bottom) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5 10.2 32.4 1.04 4.72 18.1 0.59 34.1 -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 3 3 PEG tie 1 19.31 8.53 25.84 4.82 6.45	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ \hline \\ 2804 \left(2\right) + \text{Water} \\ \hline \\ \hline \\ \hline \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ \hline \\ O_{4}\left(2\right) + \text{Water}\left(3 \\ \hline \\ \hline \\ 19.22 \\ 8.98 \\ 30.94 \\ 2.90 \\ 5.15 \\ \hline \end{array}$	$\begin{array}{c} & & & & \\ & & & & \\ & & & & \\ 10^{-9} & & & & \\ 10^{-9} & & & & \\ 1.77 \\ & & & & \\ 0.28 \\ & & & \\ 66.5 \\ & & & \\ -2.0 \\ \hline \\ (3) \\ \hline \\ (3) \\ \hline \\ \hline \\ (3) \\ \hline \\ \hline \\ (3) \\ \hline \\ (3) \\ \hline \\ \hline \\ (3) \\ \hline$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{301}$ $\frac{31}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ 38.64 \\ 0.59 \\ 2.20 \\ \hline \\ \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line length tie line longth tie line length tie line longth tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) 100 w_2 (bottom)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5 10.2: 32.4 1.04 4.72 18.1 0.599 34.1: -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 33 PEG tie 1 19.31 8.53 25.84 4.82 6.45 13.11	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ \hline -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 1.85 \\ 28.28 \\ 0.306 \\ 0.417 \\ 51.44 \\ -1.99 \\ O_{4}\left(2\right) + \text{Water}\left(3\right) \\ tie 2 \\ 19.22 \\ 8.98 \\ 30.94 \\ 2.90 \\ 5.15 \\ 14.32 \\ \end{array}$	$\begin{array}{c} & & & & & \\ & & & & & \\ & & & & & \\ 10^{-9} & & & & 1.77 \\ & & & & & \\ 1.70 & & & & & \\ 31.2 \\ & & & & & \\ 0.29 \\ & & & & \\ 66.5 \\ & & & & \\ -2.0 \\ \hline & & & & \\ (3) \\ \hline & & & & \\ \hline & & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.55 \\ & & & & \\ 48.97 \\ & & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.55 \\ & & & & \\ 48.97 \\ & & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & & \\ 18.97 \\ & & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.80 \\ & & & & \\ 18.97 \\ & & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & & \\ 18.97 \\ & & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 2.27 \times 1 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 18.97 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 18.97 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 18.80 \\ & & & \\ 18.97 \\ & & & \\ 18.80 \\ & $	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{301}$ $\frac{31}{10^{-4}}$	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ 38.64 \\ 0.59 \\ 3.30 \\ 17.29 \\ \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line length tie line longth tie line length tie line length tie line longth tie line longth tie line longth tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (top) 100 w_2 (top) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass)	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 1 19.5 10.2 32.4 1.04 4.72 18.1 0.59 34.1 -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 3 3 PEG tie 1 19.31 8.53 25.84 4.82 6.45 13.11 0.690	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 1.85 \\ 28.28 \\ 0.306 \\ 19.17 \\ 15.62 \\ 46.00 \\ 9.52 \times 10^{-3} \\ 2.14 \\ 25.26 \\ 0.417 \\ 51.44 \\ -1.99 \\ O_{4}\left(2\right) + \text{Water}\left(3\right) \\ 19.22 \\ 8.98 \\ 30.94 \\ 2.90 \\ 5.15 \\ 14.32 \\ 0.582 \\ \end{array}$	$\begin{array}{c} & & & & & \\ & & & & & & \\ & & & & & & $	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{301}$ $\frac{1}{4}$ 10^{-4}	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ 38.64 \\ 0.59 \\ 3.30 \\ 17.29 \\ 0.484 \\ \hline \end{array}$		
100 w_1 (mixture) 100 w_2 (mixture) 100 w_1 (bottom) 100 w_2 (top) 100 w_2 (bottom) phase ratio (mass) tie line length tie line slope 100 w_1 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (mixture) 100 w_2 (bottom) phase ratio (mass) tie line length tie line length tie line length tie line length tie line slope 100 w_2 (bottom) phase ratio (mass) tie line slope 100 w_2 (bottom) phase ratio (mass) tie line length	tie 1 19.07 9.34 31.57 0.33 5.01 15.82 0.600 33.06 -2.89 tie 19.5 10.2 32.4 1.04 4.72 18.1 0.59 34.1 -2.3	PEC tie 2 18.70 12.21 41.73 0.01 3.53 19.25 0.448 44.58 -2.65 PEG-2 1 5 3 1 5 0 2 3 3 PEG 2 3 3 PEG 2 3 3 PEG 2 3 3 PEG 2 3 3 PEG 2 3 3 25.84 4.82 6.45 13.11 0.690 22.05	$\begin{array}{c} -2000 \ (1) + K_2C \\ \hline tie \ 3 \\ \hline 18.35 \\ 14.97 \\ 46.22 \\ 1.14 \times 10^{-2} \\ 22.87 \\ 0.397 \\ 50.31 \\ -2.32 \\ \hline 000 \ (1) + (NH_4) \\ \hline tie \ 2 \\ \hline 19.29 \\ 12.94 \\ 40.90 \\ 0.13 \\ 2.95 \\ 21.81 \\ 0.470 \\ 44.92 \\ -2.16 \\ -2000 \ (1) + Li_2S \\ \hline \end{array}$	$\begin{array}{r} O_{3}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ \hline \\ \hline \\ 17.68 \\ 20.19 \\ 57.76 \\ 3.78 \times \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 1.85 \\ 28.28 \\ 0.306 \\ 63.53 \\ -2.18 \\ 1.85 \\ 28.28 \\ 0.306 \\ 4.17 \\ 51.44 \\ -1.99 \\ O_{4}\left(2\right) + \text{Water}\left(3\right) \\ \hline \\ 19.22 \\ 8.98 \\ 30.94 \\ 2.90 \\ 5.15 \\ 14.32 \\ 0.582 \\ 29.50 \\ \end{array}$	$\begin{array}{c} 17.3\\ 22.6\\ 59.5\\ 10^{-9} \\ 1.77\\ 1.70\\ 31.2\\ 0.29\\ 66.5\\ -2.1\\ (3)\\ \hline \\ \hline \\ 18.80\\ 18.55\\ 48.97\\ 2.27 \times 1.75\\ 29.02\\ 0.384\\ 56.04\\ -1.80\\ \hline \\ \hline \\ 19.13\\ 9.93\\ 34.50\\ 0.85\\ 4.27\\ 16.68\\ 0.543\\ 35.86\\ \hline \end{array}$	$\frac{\text{tie 5}}{34}$ $\frac{37}{59}$ 7×10^{-12} $\frac{28}{301}$ $\frac{1}{4}$ 10^{-4}	$\begin{array}{c} \text{tie 6} \\ 17.05 \\ 25.05 \\ 64.59 \\ 1.98 \times 10^{-15} \\ 1.36 \\ 33.54 \\ 0.264 \\ 72.168 \\ -2.01 \\ \hline \\ \hline \\ 18.57 \\ 21.43 \\ 53.07 \\ 3.91 \times 10^{-6} \\ 1.30 \\ 32.26 \\ 0.350 \\ 61.44 \\ -1.71 \\ \hline \\ \hline \\ \hline \\ 19.00 \\ 10.52 \\ 38.64 \\ 0.59 \\ 3.30 \\ 17.29 \\ 0.484 \\ 40.54 \\ \hline \end{array}$		

Table 3. (Continued)

	$1011304(2) \pm 0001(3)$		
tie 1 tie	2 tie 3	tie 4	tie 5
100 <i>w</i> ₁ (mixture) 18.93 18.7	78 18.67	18.53	18.45
$100w_{0}(mixture) 9.38 9.85$	5 10.92	11.36	12.01
$100w_2(ton)$ 29.09 30.7	70 33.33	34.67	36.43
$100w_{1}(top)$ 20.00 00.7 $100w_{2}(top)$ 1.32 1.21	0 69	0.62	0.48
$100w_{1}(ton)$ 1.52 1.21	2 46	2 10	1 87
$100 w_2(top)$ 3.49 3.07	2.40	2.13	1.07
$100 W_2(\text{Dottolll})$ 19.36 19.6 whose matrix (mass) 0.624 0.55	04 21.30 0 551	21.34	22.14
pnase ratio (mass) 0.034 0.05		0.520	0.300
the line length 32.09 33.3	76 -1.72		41.27
the line slope 1.75 1.	1.75	1.70	1.77
PEG-2000 (1) +	$ZnSO_4$ (2) + Water (3)		
tie 1	tie 2	tie 3	tie 4
$100 w_1$ (mixture) 18.31	18.25	18.05	18.00
$100 w_2$ (mixture) 11.87	12.52	13.07	13.72
$100 w_1(top)$ 35.54	37.76	39.19	39.98
$100 w_1$ (bottom) 0.38	0.31	0.26	0.16
$100 W_2(top)$ 2.27	1.89	1.68	1.57
$100w_2$ (bottom) 21.86	22.29	22.66	23.59
phase ratio (mass) 0.510	0.479	0.457	0.448
tie line length 40.26	42.65	44.23	45 51
tie line slope -1.79	-1.84	-1.85	-1.81
EEC 2000 (1) +	$N_{2}OH(2) \perp W_{2}$		
	tia	. 9	tio 2
	10	, <u>~</u> 00	19.09
$100 w_1(\text{mixture})$ 19.25	18.	90 F	18.08
$100 W_2(\text{mixture})$ 7.27	8.9	5	10.58
$100 w_1(top)$ 40.92	49.	41	54.45
$100 w_1$ (bottom) 0.57	0.0	50	2.32e-3
$100 w_2(top)$ 2.65	1.8	0	1.39
$100 w_2$ (bottom) 11.26	13.	39	15.38
mass ratio 0.463	0.3	83	0.343
tie line length 41.26	50.	71	56.21
tie line slope -4.68	-4	.26	-3.89
Table 4. Effective Excluded Volume As Determined by Regression of Lilley's Statistical Geometry Model on the	40 ·		
PEG + Salt ABS			
apparent scaled molar regression	30 -		
salt $ ext{EEV} imes 10^6$ mass coefficient,			
system (kg/mol) (g/mol) r ²			
7-50 21 72 161 46 0.02			
LIISO4 51.75 101.40 0.92 V DO 49.40 919.97 0.09	• 20 ·		
K_3FU_4 48.40 212.27 0.93	10		
MnSO ₄ 28.66 151.01 0.95			
$L_{12}SO_4$ 25.54 109.95 0.95			
NaOH 12.74 40.00 0.97	10 -	- & ///	
Na ₂ CO ₃ 26.39 103.99 0.97		ا هم ۱	
(NH ₄) ₂ SO ₄ 31.01 132.29 0.86		. * * *	
that the calt phase is virtually free of DEC at long the line	0 -	- 	Ale
that the salt phase is virtually free of PEG at long the line			20 25
lengths. This also means that the salting-out constant of	-	0 5 10 15	20 25
the Setchenow equation (eq 3) is not a constant, indicating		100 w	
a change in activity coefficient over these extended tie line		100	
longths. Those data are not shown but may assily be			
calculated from Table 3.	(2) ABS, showin titration (●), the	g the binodal curve det fitted cloud point curve, a	ermined by cloud point and the overall and node
W_i^{T} , \mathbb{R} , \mathbb{T}	compositions (O)	of several fitted tie line	S.
$\ln \frac{1}{-B} = \beta_i + k_j^i (k_j^B - w_j^T) \tag{3}$			
W_{i}	poor fit from a	practical point of view	. However, the single
	fitted naramete	er should, at constant	PEG molar mass he
In as 2 wronnegents the mass concentrations of the two	roloted to the	alting out strongth	f the solt Figure 10
in eq. 5, w represents the mass concentrations of the two		saiding-out strength (n ule sait. Figure 10

species i and j in the two phases, T and B. The k term is the salting-out coefficient, and β is a constant related to the activity coefficient.

We have also treated the data using an equation derived from statistical geometrical considerations by Lilley (eq 2). The results, which are given in Table 4, show the effective excluded volume (EEV or V*, the fitted parameter of eq 2) and the regression coefficient. The latter indicates a rather shows the EEV in relation to the molar mass of the ABS

phase-forming salts examined. It appears that there is a close relationship between the molar mass of the salt and its excluded volume. Unfortunately, this can only really be considered an artifact of the Lilley equation, since such a relationship cannot in general be true. Consider for instance the well-known exception in many attempts to correlate the Hofmeister series represented by CaCl₂



Figure 8. Phase diagram in w/w % of the PEG-2000 (1) + $ZnSO_4$ (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.



Figure 9. Phase diagram in w/w % of the PEG-2000 (1) + NaOH (2) ABS, showing the binodal curve determined by cloud point titration (\bullet), the fitted cloud point curve, and the overall and node compositions (\bigcirc) of several fitted tie lines.



Figure 10. Effective excluded volume from Lilley's statistical geometry as determined for various PEG + salt ABS in relation to salt molecular size.

compared to NaCl, for example, in the treatment of protein precipitation by Mellander and Horvath³⁶ or in the depression of PEG cloud point temperature with salt concentration in the data reported by Bailey.³⁷

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